

Low-Noise and Long-Range PIR Sensor Conditioner Circuit with MSP430™ Smart Analog Combo



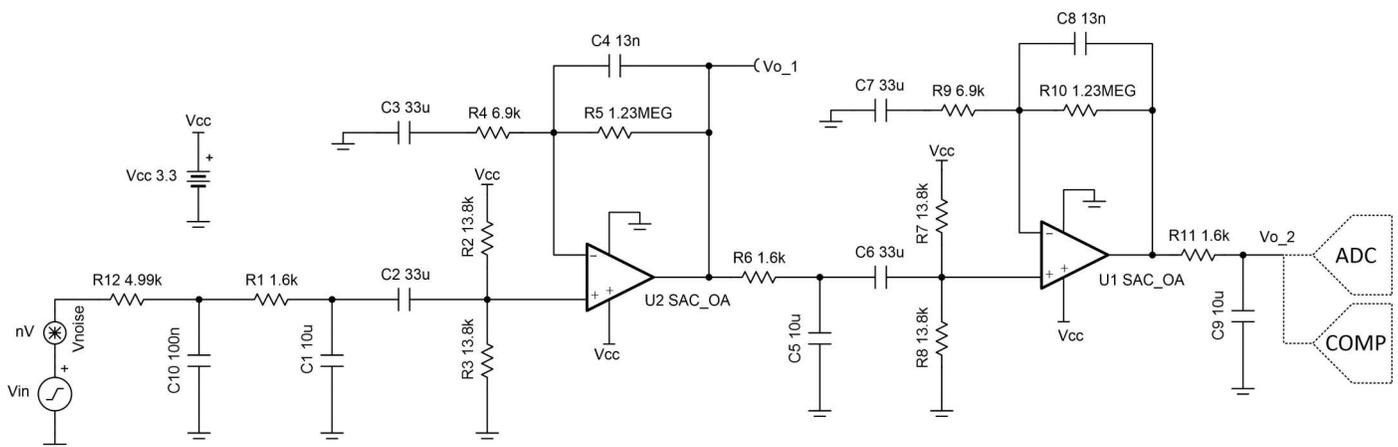
Design Goals

AC Gain	Filter Cut-Off Frequency		Supply	
90 dB	f_L	f_H	V_{CC}	V_{EE}
	0.7 Hz	10 Hz	3.3 V	0 V

Design Description

Some MSP430™ microcontrollers (MCUs) contain configurable integrated signal chain elements such as op-amps, DACs, and programmable gain stages. These elements make up a peripheral called the Smart Analog Combo (SAC). For information on the different types of SACs and how to leverage their configurable analog signal chain capabilities, visit [MSP430 MCUs Smart Analog Combo Training](#). To get started with your design, download the [Low-Noise Long-Range PIR Sensor Conditioner Circuit Design Files](#).

This design leverages two of the four integrated op-amp blocks (SACs) in the [MSP430FR2355](#) MCU. Two SAC_L3 peripherals are configured as cascaded op-amps in general-purpose mode to amplify and filter the signal from a passive infrared (PIR) sensor. The circuit includes multiple low-pass and high-pass filters to reduce noise at the output of the circuit to be able to detect motion at long distances and reduce false triggers. The output of the second-stage op-amp in this circuit can be internally or externally connected to other integrated peripherals in the [MSP430FR2355](#) MCU. For example, the analog-to-digital converter (ADC) window comparator can sample this output periodically (with no CPU intervention) and trigger an interrupt when the signal crosses a threshold, indicating motion or an alert.



Design Notes

- The common-mode voltage and output-bias voltage are set using the resistor dividers between R_2 and R_3 (and R_7 and R_8).
- Two or more amplifier stages must be used to allow for sufficient loop gain.
- Additional low-pass and high-pass filters can be added to further reduce noise.
- Capacitors C_4 and C_8 filter noise by decreasing the bandwidth of the circuit and help stabilize the amplifiers.
- RC filters on the output of the amplifiers (for example, R_6 and C_5) are required to reduce the total integrated noise of the amplifier.
- The maximum gain of the circuit can be affected by the cut-off frequencies of the filters. The cut-off frequencies may need to be adjusted to achieve the desired gain.
- For this design, two SAC_L3 peripherals in the [MSP430FR2355](#) MCU are configured as cascaded op-amps in general-purpose mode.
- This design can also be implemented by using the transimpedance amplifier (TIA) and SAC_L1 peripheral in the [MSP430FR2311](#) MCU for the cascaded op-amps, but since the maximum input voltage of the TIA is limited to $VCC/2$, the common-mode voltage and gain should be limited accordingly.
- The [Low-Noise Long-Range PIR Sensor Conditioner Circuit Design Files](#) include a code example demonstrating how to properly configure the SAC_L3 and ADC window comparator peripherals in the [MSP430FR2355](#) MCU.

Design Steps

1. Choose large-valued capacitors C_1 , C_5 , and C_9 for the low-pass filters. These capacitors should be selected first because large-valued capacitors have limited standard values to select from compared to standard resistor values.

$$C_1 = C_5 = C_9 = 10\mu\text{F}$$

2. Calculate resistor values for R_1 , R_6 , and R_{11} to form the low-pass filters.

$$R_1 = R_6 = R_{11} = \frac{1}{2\pi \times f_H \times C_1} = \frac{1}{2\pi \times 10\text{Hz} \times 10\mu\text{F}} = 1.592\text{k}\Omega$$

$$\text{Choose } R_1 = R_6 = R_{11} = 1.6\text{k}\Omega \quad (\text{Standard value})$$

3. Select capacitor values for C_2 , C_3 , C_6 , and C_7 for the high-pass filters.

$$C_2 = C_3 = C_6 = C_7 = 33\mu\text{F}$$

4. Calculate the resistor values for R_4 and R_9 for the high-pass filters.

$$R_4 = R_9 = \frac{1}{2\pi \times f_L \times C_2} = \frac{1}{2\pi \times 0.7\text{Hz} \times 33\mu\text{F}} = 6.89\text{k}\Omega$$

$$\text{Choose } R_4 = R_9 = 6.9\text{k}\Omega \quad (\text{Standard value})$$

5. Set the common-mode voltage of the amplifier to mid-supply using a voltage divider. The equivalent resistance of the voltage divider should be equal to R_4 to properly set the corner frequency of the high-pass filter.

$$R_2 = R_3 = R_7 = R_8 = 2 \times R_4 = 2 \times 6.9\text{k}\Omega = 13.8\text{k}\Omega$$

$$\text{Choose } R_2 = R_3 = R_7 = R_8 = 13.8\text{k}\Omega \quad (\text{Standard value})$$

6. Calculate the gain required by each gain stage to achieve the total gain requirement. Distribute the total gain target of the circuit evenly between both gain stages.

$$\text{Gain} = \frac{90\text{dB}}{2} = 45\text{dB} = 177.828\frac{\text{V}}{\text{V}}$$

7. Calculate R_5 to set the gain of the first stage.

$$R_5 = (\text{Gain} - 1) \times R_4 = (177.828\frac{\text{V}}{\text{V}} - 1) \times 6.9\text{k}\Omega = 1.22\text{M}\Omega$$

$$\text{Choose } R_5 = 1.23\text{M}\Omega \quad (\text{Standard value})$$

8. Calculate C_4 to set the low-pass filter cut-off frequency.

$$C_4 = \frac{1}{2\pi \times f_H \times R_5} = \frac{1}{2\pi \times 10\text{Hz} \times 1.23\text{M}\Omega} = 12.939\text{nF}$$

$$\text{Choose } C_4 = 13\text{nF} \quad (\text{Standard value})$$

9. Since the gain and cut-off frequency of the first gain stage is equal to the second gain stage, set all component values of both stages equal to each other.

$$R_1 = R_6 = 1.6\text{k}\Omega$$

$$R_7 = R_8 = 13.8\text{k}\Omega$$

$$R_9 = R_4 = 6.9\text{k}\Omega$$

$$R_{10} = R_5 = 1.23\text{M}\Omega$$

$$C_8 = C_4 = 13\text{nF}$$

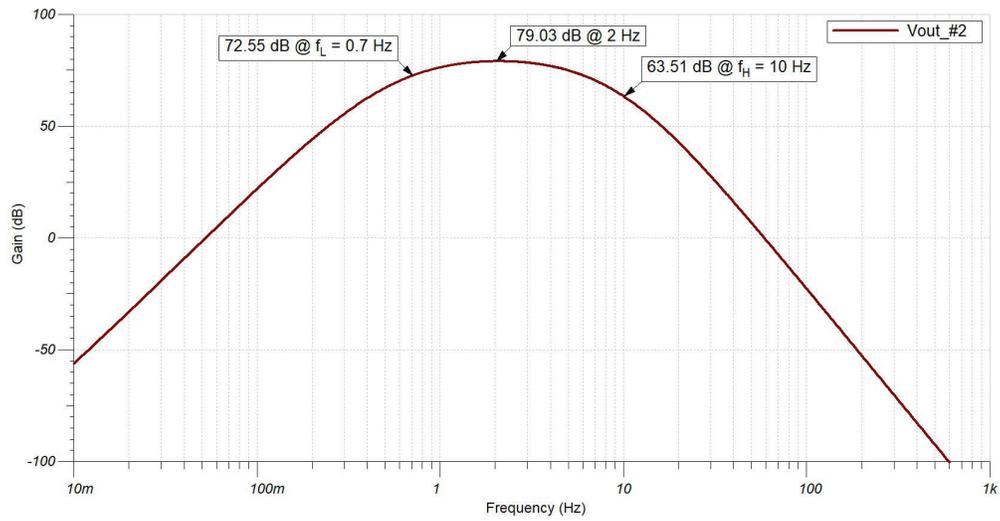
10. Calculate R_{11} to set the cut-off frequency of the low-pass filter at the output of the circuit.

$$R_{11} = \frac{1}{2\pi \times f_H \times C_9} = \frac{1}{2\pi \times 10\text{Hz} \times 10\mu\text{F}} = 1.592\text{k}\Omega$$

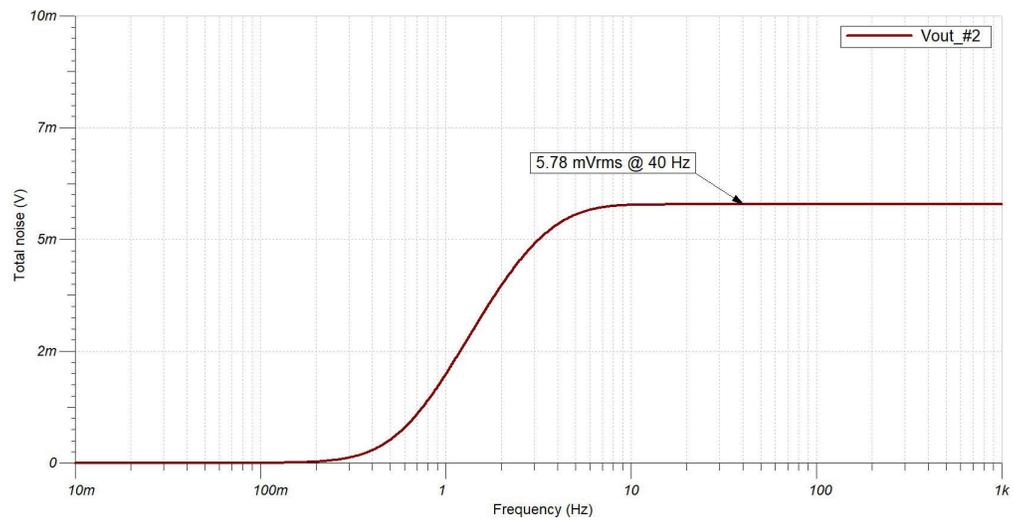
$$\text{Choose } R_{11} = 1.6\text{k}\Omega \quad (\text{Standard value})$$

Design Simulations

AC Simulation Results



Noise Simulation Results



Target Applications

- [Motion detector](#)
- [Occupancy detection](#)
- [Analog security camera](#)
- [IP network camera](#)
- [Lighting sensor](#)
- [Thermostat](#)
- [Video doorbell](#)

References

1. [Low-Noise Long-Range PIR Sensor Conditioner Circuit Design Files](#)
2. [Analog Engineer's Circuit Cookbooks](#)
3. [MSP430FR2311 TINA-TI Spice Model](#)
4. [How to Use the Smart Analog Combo in MSP430™ MCUs](#)
5. [MSP430 MCUs Smart Analog Combo Training](#)

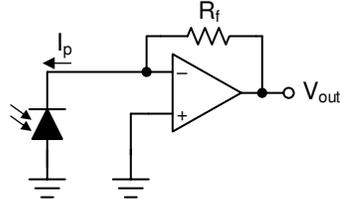
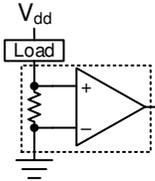
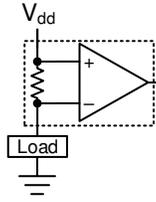
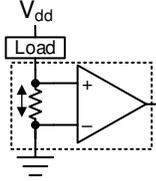
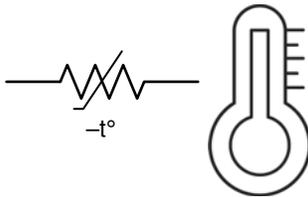
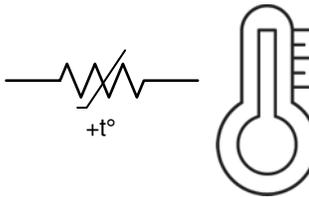
Design Featured Op Amp

MSP430FRxx Smart Analog Combo		
	MSP430FR2311 SAC_L1	MSP430FR2355 SAC_L3
V_{CC}	2.0 V to 3.6 V	
V_{CM}	-0.1 V to V _{CC} + 0.1 V	
V_{out}	Rail-to-rail	
V_{os}	±5 mV	
A_{OL}	100 dB	
I_q	350 μA (high-speed mode)	
	120 μA (low-power mode)	
I_b	50 pA	
UGBW	4 MHz (high-speed mode)	2.8 MHz (high-speed mode)
	1.4 MHz (low-power mode)	1 MHz (low-power mode)
SR	3 V/μs (high-speed mode)	
	1 V/μs (low-power mode)	
Number of channels	1	4
	MSP430FR2311	MSP430FR2355

Design Alternate Op Amp

MSP430FR2311 Transimpedance Amplifier	
V_{CC}	2.0 V to 3.6 V
V_{CM}	-0.1 V to $V_{CC}/2$ V
V_{out}	Rail-to-rail
V_{os}	± 5 mV
A_{OL}	100 dB
I_q	350 μ A (high-speed mode)
	120 μ A (low-power mode)
I_b	5 pA (TSSOP-16 with OA-dedicated pin input)
	50 pA (TSSOP-20 and VQFN-16)
UGBW	5 MHz (high-speed mode)
	1.8 MHz (low-power mode)
SR	4 V/ μ s (high-speed mode)
	1 V/ μ s (low-power mode)
Number of channels	1
MSP430FR2311	

Related MSP430 Circuits

<p>Low-noise and long-range PIR sensor conditioner circuit</p> 	<p>Bridge amplifier circuit</p> 	<p>Transimpedance amplifier circuit</p> 
<p>Single-supply, low-side, unidirectional current-sensing circuit</p> 	<p>High-side current sensing with discrete difference amplifier circuit</p> 	<p>Low-side, bidirectional current-sensing circuit</p> 
<p>Half-wave rectifier circuit</p> 	<p>Temperature sensing with NTC thermistor circuit</p> 	<p>Temperature sensing with PTC thermistor circuit</p> 

Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from November 15, 2019 to March 6, 2020	Page
• Added <i>Related MSP430 Circuits</i> section.....	1

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